

10/505356

**Nitinol Ice Blades**

This is related U.S. Provisional Application No. 60/358,988 filed on February 21, 2002 and entitled "Nitinol Ice Blades" and to U.S. Provisional Application Nos. 5 60/210,902 and 60/265,562 filed on June 11, 2000 and January 31, 2001, respectively, and U.S. Patent Applications No. 09/879,371 filed on June 11, 2001, which issued as U.S. Patent No. 6,422,010 on July 23, 2002, entitled "Manufacturing of Nitinol Parts and Forms", and U.S. Provisional Applications 60/036,784, 60/029,251, 60/011, 648 filed on Jan. 28, 1997, Oct. 24, 1996, and Feb. 14, 1996, 10 respectively, perfected as PCT/US97/02324 on Feb. 14, 1997 and U.S. Patent Application No. 09/125,218, issued as Patent No. 6,293,020 on Sept. 25, 2001, and Divisional Application 09/926,978 filed on Sept. 24, 2001.

This invention relates to Nitinol ice skate blades that have superior erosion resistance, toughness, low sliding friction on ice, and excellent corrosion resistance, 15 and to processes for produce them.

**BACKGROUND OF THE INVENTION**

Ice skating is a widely popular sport in many countries. The evolution of skating has led to many innovative changes in the hardware used in this sport. These 20 innovations include improved designs for skate blades and the metals used for the blades. Existing ice skate blades are presently manufactured from high carbon steels, stainless steels or titanium. Each of these materials has characteristics that are undesired. Corrosion resistance is an important characteristic for ice skate blades. As a blade corrodes, the cutting edge deteriorates, thus becoming dull. When skate 25 cutting edges are dull, they do not effectively cut into the ice. Sharp cutting edges are important, especially when a skater is making turns. Presently, it is not uncommon for hockey players to grind their skates twice during a competition game. All skating rinks have grinding equipment to provide for the regrounding of blades. Improvements in the ability of ice skate blades to retain a sharp edge and resist corrosion would be an 30 important factor in the sports of hockey, speed skating and figure skating.

High carbon steels are subject to corrosion and thus dulling of the running surface of the blade. Stainless steels have better corrosion resistance properties than

the high carbon steel blades however, are still subject to corrosion. Corrosion is the primary reason for the dulling of steel ice skate blades. Thus, if a blade had good corrosion resistance, the time between re-grinding could be reduced.

Ice skate blades produced from high carbon steel are normally plated with chrome or other corrosion resistant materials. This plating however, cannot be applied to the running surface of the blade as they are constantly being re-ground to produce two ice cutting edges. Stainless steel blades have better corrosion resistance than high carbon steel, but in order to be heat treatable to high hardness, substantial carbon content in the alloy is required. This high carbon content increases the potential for corrosion.

Titanium skate blades do have good corrosion resistance properties. However, titanium cannot be processed to have high hardness. Titanium can be processed to have a maximum hardness of ~38 Rockwell C.

An important consideration when selecting a skate blade material, besides hardness of the metal surface that rides on the ice, is brittleness. The skate blade material must be hard enough to minimize erosion of the blade, but not so hard as to be brittle. Hockey blades, especially, must be malleable enough to absorb impacts without shattering.

A third factor, not commonly considered for conventional skate blade design, is the coefficient of friction of the blade on the ice. Skate blades concentrate the weight of the skater in a small area and the resulting pressure produces a film of water, which lubricates the skate blade as it slides over the ice surface. However, there is solid ice contact on skate blade edges during skating, particularly during turning and hard edging while accelerating forward. Improvements to the coefficient of friction of the skate blade on the ice would improve the speed and smooth feel of the skates and would be an improvement much welcomed by skaters.

The same characteristics would also be useful for other ice sliding equipment such as sleds and ice boats, and on other sporting vehicles intended for use on ice, such a luge, bobsled and skeleton.

30

#### SUMMARY OF THE INVENTION

Accordingly, this invention provides a Nitinol ice blade and processes for manufacturing a Nitinol ice blade that provides capabilities unavailable in current

blades or any known variant of current blades. In particular, I contemplate the use of Nitinol as hockey, figure and speed ice skating blades. Although both the Type 55 and Type 60 Nitinol material can be used for blade fabrication, the preferred material is the Type 60. Type 60 can be processed to have high hardness (up to Rockwell 5 62C), has excellent toughness properties, a weight approximately 16% less than steel, superior corrosion resistance, and can be polished to have mirror finishes.

The Nitinol skate blades of this invention run faster on the ice, turn better, and last longer between sharpenings than any skate blade ever known to man. Moreover, they are lighter and chatter less on the ice than current state-of-the-art skate blades.

10 These Nitinol skate blades are corrosion resistant so they will not rust like steel blades between uses, and they have a lower Young's modulus and a higher damping capacity than steel, so they tend to hold their grip on the ice better than steel blades. They have a lower coefficient of friction on the ice than steel and they can be heat treated to have a very smooth and hard oxide finish on the side edges that is even 15 harder and smoother, and has a lower coefficient of friction to produce exceptional running properties on the ice. Type 60 Nitinol can be processed to have a hardness of up to 62 Rockwell C, superior erosion resistance, toughness, and is virtually corrosion proof in the environment of a skating rink. Type 60 Nitinol blades can run on ice approximately five times longer than existing steel blades before re-grinding is 20 required.

The invention includes processes for manufacturing Type 60 Nitinol skate blades. They are cut by available economical cutting processes such as laser or abrasive water jet from rolled Type 60 Nitinol sheet or extruded Type 60 Nitinol bars, and are heat treated to reduce brittleness and improve toughness and impact 25 strength, and give the skate blade an elastic property which I call "ultraelasticity".

The part may be machined to reduce it to near net size, and may be ground to reduce the part to the exact specified part size. For example, flat stock can be surface ground. For parts requiring a smooth surface finish, polishing or lapping provides the specified surface finish on the part, down to 0.5 microinch RMS or finer. The part may 30 be heat treated to obtain the desired hardness, from RC40 to RC65.

An integral surface oxide of any of several colors can be formed on the surface of the part. The oxide surface may itself be polished to an even finer surface finish. These process elements may all be used to produce a particular part that requires the

characteristics provided by each process element, and they may be used in combinations that omit particular process elements or substitute others to give the desired characteristics of the part.

The unique physical characteristics of Type 60 Nitinol make it the ideal material  
5 to be used for ice blades, and ice skate blades, in particular. The corrosion resistance  
of the material ensures that blades made from Nitinol will never rust when used on ice.  
Corrosion of existing steel and stainless steel is a major cost factor to the ice sport  
industry. Presently, the manufacturers of high carbon steel blades apply chrome  
plating to the blades in an attempt to reduce the effect of corrosion. The problem this  
10 approach is that the runner (bottom) of the blades are periodically ground to  
resharpen the edges, which of course removes the chrome plating. After exposure to  
the ice (water) the bottom of the blade corrodes, and thus dulls rapidly. This corrosion  
process also occurs on stainless steel blades, although it takes longer. Salt fog  
corrosion tests performed on high-carbon steel showed signs of corrosion in salt water  
15 within eight minutes, and four hours on 440C type stainless steel. The same tests  
performed on Type 60 Nitinol showed no corrosion after several thousand hours of  
exposure to salt fog.

#### **DESCRIPTION OF THE DRAWINGS**

20 The invention and its many attendant benefits and advantages will become  
better understood upon reading the following detailed description of the preferred  
embodiments in conjunction with the following drawings, wherein:

Fig. 1 is an exploded elevation of a hockey ice skate having a Nitinol skate  
blade in accordance with this invention;

25 Fig. 2 is an exploded elevation of a hockey ice skate blade holder and skate  
blade exploded out of the holder;

Fig. 3 is an end view of the skate blade shown in Fig. 2;

Fig. 4 is an end elevation of the skate blade mounted in the holder shown in  
Fig. 2;

30 Fig. 5 is a is an elevation of a figure skate having a Nitinol skate blade in  
accordance with this invention;

Fig. 6 is a sectional elevation of the Nitinol skate blade shown in Fig. 5;

Fig. 7 is an end sectional elevation of one version of the skate blade shown in Fig. 5;

Fig. 8 is an end sectional elevation of another embodiment of the skate blade shown in Fig. 5;

5 Fig. 9 is an elevation of a speed skate blade in accordance with this invention; and

Fig. 10 is a sectional elevation of the skate blade shown in Fig. 9.

#### **DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS**

10 Referring now to the drawings, wherein like reference numerals designate the same or corresponding parts, and more particularly to Figs. 1 and 2 thereof, a hockey skate 20 is shown having a boot 23 and a blade holder 26 in which a skate blade 30 in accordance with this invention is removably mounted. The skate blade 30 has attachment structures 32 for engaging complementary structures 34 on the blade holder 26 to securely attach the skate blade 30 to the blade holder 26. These structures 32 and 34 are conventional and are well known to those skilled in the art.

15 20 A figure skate blade 40, shown in Fig. 5, has a Nitinol edge 44 attached to a Titanium or stainless steel blade body 42 by welding, such as laser welding. The edge 44 can also be fitted into a groove in the blade body 42 as shown in Fig. 7, or can be fitted around the blade body in a channel shaped edge 44' as shown in Fig. 8.

A speed skate blade 50, shown in Fig. 10, has a skate body 52 with conventional attachment structure for attaching the blade 50 to a speed skate boot. It could alternatively have the now conventional clap skating structure that attaches the blade to the skate boot with a pivotal attachment. A Nitinol edge structure 56 fits into 25 a groove in the skate blade 50 is attached to the blade 50 by attachment structure 58.

As used herein, the term ice blade and ice skate blade is intended to encompass other types of apparatus and equipment that slide on ice, such as sleds and ice boats, and sporting vehicles intended for use on ice, such a luge, bobsled and skeleton.

30 Nitinol is a nickel-titanium intermetallic compound invented at the Naval Ordnance Laboratory in the early 1960's. It is a material with useful properties, but manufacturers who have worked with it have had little success in making Nitinol parts and semi-finished forms. Because Nitinol is so extremely difficult to form and

machine, workers in the metal products arts usually abandoned the effort to make products out of anything except Type 55 Nitinol drawn wire because the time and costs involved did not warrant the paltry results they were able to obtain.

Type 60 Nitinol (60% Nickel and 40% Titanium by weight), has many properties that are unrecognized as of potential value. It can be polished to an extremely smooth finish, less than 1 microinch rms. It is naturally hard and can be heat treated to a hardness on the order of 62Rc or higher. It can be processed to have a very hard integral complex oxide surface that can itself be polished to an even smoother surface than the parent metal. It is non-magnetic, immune to corrosion from most common corrosive agents, and can be treated to have a high yield strength and toughness, even at elevated temperatures. It is 26% lower density than steel for weight sensitive applications such as aircraft, satellites and spacecraft. However, there has hitherto been little effort in making useful parts out of Type 60 Nitinol because it is so difficult to work, because it was known to be brittle, and because there has been no known method to make parts and forms out of it.

Type 60 Nitinol can be hot rolled from a cast billet by successive hot passes through a rolling mill. It can be successfully rolled at a temperature of about 900°C to 950°C to a reduction of at least about 2% per pass in the dimension of the hot-working. The polled sheet is normally hard and brittle without subsequent heat treatment.

To make ice blades, as illustrated in Figs. 11 and 12, a Type 60 Nitinol sheet or plate 60 that has been hot-worked as noted above, or an extruded bar 62 shown in Fig. 12, is selected and blade blanks 64 are cut out of the sheet. They are cut by available economical cutting processes such as laser or abrasive water jet from rolled Type 60 Nitinol sheet 60 or extruded Type 60 Nitinol bars 62, and are heat treated, as described below, to reduce brittleness and improve toughness and impact strength, and give the skate blade an elastic property which I call "ultraelasticity".

Nitinol ice skate blades must be processed to be both tough and hard. The hardness and toughness of the blades is achieved in accordance with this invention by a heat treatment process. The optimum hardness of the blade strong back is 48 to 53 Rockwell C. The hardness of the bottom of the runners can be processed to have a higher hardness (up to 62 Rc) if desired.

The high toughness properties of Type 60 Nitinol can be achieved by heating the blade blanks in an oven to between 600°C and 800°C, preferably about 700°C ±20°C, and then rapidly quenching the blank in a coolant such as oil or water. This yields the desired characteristics of high hardness and toughness for the blade  
5 blanks. The optimum hardness for the blades is 49 to 53 Rockwell C and a yield strength of over 120,000 psi.

The surface of the blade that contacts the ice can be heat treated to have high hardness, up to 62 Rockwell C. The process consists of heat sinking the strong back of the knife and heating only the contact surface to approximately 900 to 1000  
10 degrees C°, for example, with an acetylene torch, induction coil, or other localized heating process, and then rapidly quenching the blade in water or oil.

The blade blanks 64 are finish ground to the desired final dimensions to fit properly in the blade holders 26. Prior to grinding the skate blade blanks 64 to the desired thickness, they should be flattened. Type 60 Nitinol parts may be shaped to a desired contour without spring-back by a process involving forming the part to the desired contour and heat treating it while holding it at the desired contour. One technique for performing this process is to heat the blade  
15 blanks in a furnace or oven at a temperature of 600°C-800°C, preferably 700C°. The skate blade blanks are laid onto a thick steel plate, having a flat top surface, in the furnace, and another thick steel plate, having a flat bottom surface, is placed on top of the blade blanks. The  
20 assembly is inserted in a preheated oven and, after temperature equalization, the parts are held at the 700°C temperature for a minimum of fifteen minutes. The blade blanks are then removed and immediately quenched in a water bath. The blade blanks should be held vertical when quenched in the water to minimize warping of the blade from uneven cooling. It is also desirable that the time between removal of the blade from the furnace and quenching be as  
25 short as possible. The time lag between furnace removal and quenching should be within about twenty seconds, preferably within 15 seconds from removal from the oven. In order to minimize the time lag between removal of the blanks from the oven and the quenching operation, it is convenient to locate the quenching tank close to the oven. This short lag time is useful to maintain the temperature of the blade close to 700°C at the start of the quench  
30 process. This process aligns the crystals within the material and produces a flat tough Nitinol ice blade. The hardness of the blade at this point in the manufacturing process is about 48 to 51 Rockwell C.

The flat blade blank is now ready to be ground to the required thickness. The preferred method to grind the blades is to run them through a "timesaver machine", which is a large belt grinder. To obtain a good finish on each side of the blade they should be ground on both sides. The preferred grinding belts to be used are those made from a grinding media called Cubatron, 5 a 3M company product. Cubatron belts of 60 grit are preferred, although other grid sizes can be used. A light pressure and shallow grinding passes are preferred because they produce little heat increase and do not cause significant rounding of the corners. When the blades are at the required thickness, final polishing may be accomplished using another 3M timesaver belt called Trizak. Other types of grinding media can also be used obtain the required blade 10 thickness, however the above described grinding media is preferred.

Upon completion of the above grinding operations the blades are ready for final processing. The final processes insure that all metallurgical changes produced by the cold work that was applied by the timesaver grinding operations is removed, applies the black oxide finish onto the surface of the blades, and insures toughness in the blades.

15 This final process is identical to the heat treatment used to flatten the blade. All residue from the grinding operations is removed prior to the blades being installed in the oven. The oven is preheated to the 700°C, the blades installed between the two steel plates with flat facing surfaces, and the temperature held for approximately fifteen minutes after equalizing. The blades are then removed and quenched as described above.

20 A hard and slippery black oxide finish is produced with this process. The oxide finish may then be polished to an extremely smooth finish using a buffing wheel with diamond paste or jewelers rouge.

25 The oxide finish produced during the above-described processes is hard and non-electrically conductive, which prevents conventional electro chemical etching processes to be used to apply engraving on the blades. Logos, part numbers, or designs on the blades may be applied after formation of the oxide surface material by laser engraving, or may be applied after polishing and before oxide formation by electro-chemical engraving.

30 Type 60 Nitinol skate blades rarely, if ever, need sharpening. The ice-contact edge is so hard and abrasion resistant, that there is very little abrasive wear of the edge material. Moreover, the material is essentially corrosion-proof, so there is no significant corrosion of the ice-contacting edges, which is the primary cause of edge dulling in conventional skate blades. However, grinding of the running surfaces of the

skate blades is necessary during manufacturing and may occasionally be desirable after an extended period of hard use. On some blades a hollow grind is used, for example hockey skate blades. On other types of blades a flat or wedge grind is preferred. Grinding and final forming of the blades may be performed on a

- 5 conventional skate blade sharpening machine such as a "Blademaster" three station  
skate sharpening machine made by Guspro Inc. in Chatham, Ontario, Canada.  
Conventional skate blade grinding equipment, such as the Blademaster, uses silicon  
carbide blades and diamond hones for the final pass. For Nitinol skate blades in  
accordance with this invention, the process is similar but differs in significant aspects,  
10 noted below. Conventional blade grinding wheels may be used to grind the Type 60  
Nitinol skate blades, but the process is lengthy and the conventional grinding wheels  
wear down quickly. Cubitron grinding wheels, newly available from Cincinnati Milicron  
Company in Cincinnati, Ohio, are preferred. To minimize excessive heating of the  
skate blade bottom edge during grinding, it is preferable to grind in rapid shallow  
15 passes of about 0.002"-0.003". A diamond hone may be used as a final pass to  
produce a very smooth finish and especially sharp edges. The diamond hone may  
also be used to sharpen the blade edges after extended use, but should be applied  
with light pressure to avoid pulling the diamond particles out of the hone.

Permanent marking of the blades, part numbers, logos, serial numbers etc, can  
20 be accomplished using electro-chemical etching or laser engraving processes. If  
chemical etching is to be used, the markings should be applied prior to the application  
of the oxide film because the oxide is an effective electrical current isolator and  
interferes with the electro-chemical etching process. Laser etching processes  
however, work well on both the uncoated and coated material.

25 The ultraelastic Type 60 Nitinol workpiece may be heat treated to a desired  
combination of hardness and elasticity. For example a hardness of about 58RC-64RC  
may be obtained by heating it to about 900°C-950°C and then quenching in water or  
other coolant such as oil to cool it quickly to a temperature below about 500°C. The  
coolant should be agitated or the part moved in the coolant bath to ensure a flow of  
30 coolant over the surface of the part to ensure even cooling and prevent development  
of an insulating steam cushion over portions of the part. The hardness can be tailored  
by the temperature of the initial heating. Rapid quenching produces a surface

hardness of about 58-64RC at some sacrifice to the elasticity of the material. The strength of the ultraelastic Type 60 Nitinol heat treated to about 50-55 Rockwell C and a strength of about 140,00 - 155,000 psi and has an elastic strain capability of about 3% up to about 6%.

- 5        To retain the ultraelastic properties in a portion of the workpiece but high hardness in other portions such as the edge of a ice skate blade, the portion that need not be hardened can be clamped in a heat sink and the other portion, such as the ice-contacting edge, is heated to a hardening temperature of 900°C-950°C and then rapidly quenched in water or other coolant. The heat sink prevents the unhardened  
10      portion from being heated to the hardening temperature so it retains its ultraelastic properties.

Tests performed on 60 Nitinol Hockey blades showed substantially improved results. Hockey skaters stated the blades provided improved turning and much higher speeds on the ice. The testers also used the blades for extended periods of time  
15      without the need for frequent re-sharpening.

Obviously, numerous modifications and variations of the preferred embodiment described above are possible and will become apparent to those skilled in the art in light of this specification. For example, the ice skating blade in accordance with this invention could be used for improved speed and control on sleds and ice boats, and  
20      on other sporting vehicles intended for use on ice, such a luge, bobsled and skeleton. Moreover, many functions and advantages are described for the preferred embodiment, but in many uses of the invention, not all of these functions and advantages would be needed. Therefore, I contemplate the use of the invention using fewer than the complete set of noted features, process steps, benefits, functions and  
25      advantages. For example, all the process elements may be used to produce a particular part that requires the characteristics provided by each process element, or alternatively, they may be used in combinations that omit particular process elements or substitute others to give the desired characteristics of the part. Moreover, several species and embodiments of the invention are disclosed herein, but not all are  
30      specifically claimed, although all are covered by generic claims. Nevertheless, it is my intention that each and every one of these species and embodiments, and the equivalents thereof, be encompassed and protected within the scope of the following

claims, and no dedication to the public is intended by virtue of the lack of claims specific to any individual species. Accordingly, it is expressly intended that all these embodiments, species, modifications and variations, and the equivalents thereof, in all their combinations, are to be considered within the spirit and scope of the invention as defined in the following claims, wherein I claim: